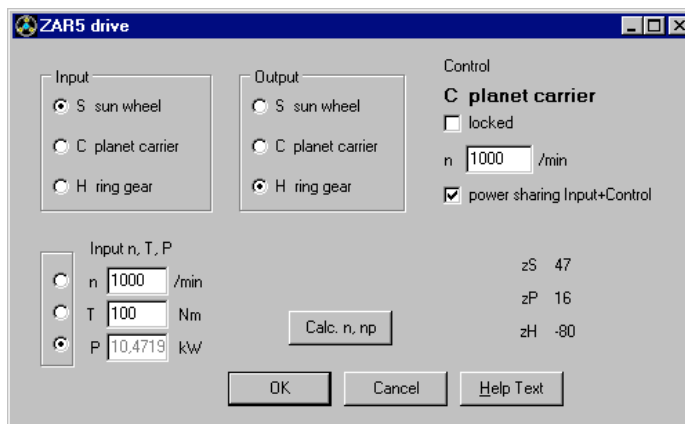


by Fritz Ruoss

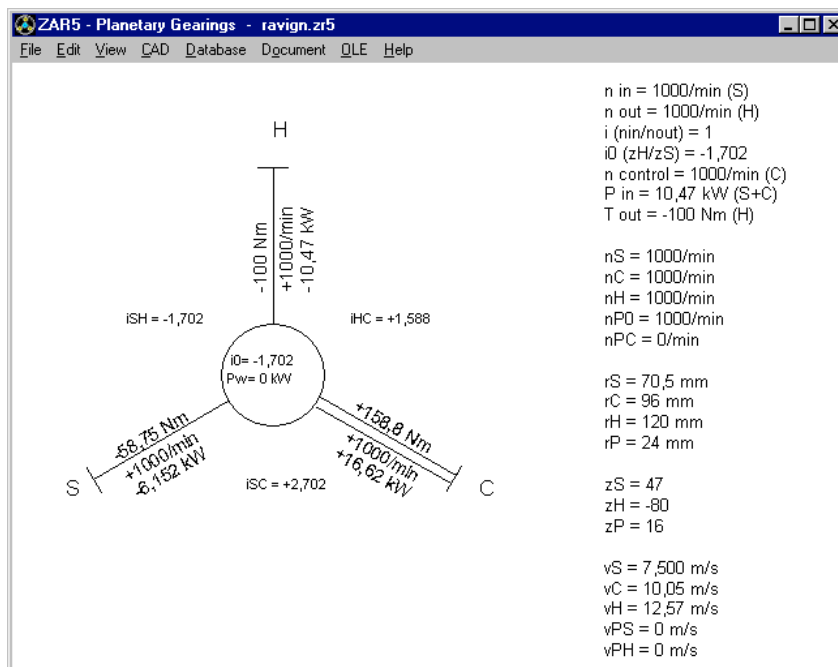
ZAR5: Power shearing (driving shaft + control shaft) as option

Sun gear, planet carrier and ring gear are connected with driving shaft (input), driven shaft (output) and control shaft (control). If control shaft is locked, power flows from input shaft to output shaft. If input shaft and control shaft are connected (for direct transmission $i=1$) or input shaft and control shaft are driven by the same motor with different speed (i.e. Lepelletier planet gear set), power will be shared between input shaft and control shaft ($P_{input} + P_{control} = P$), check "power sharing Input+Control". If not checked, full power always flows to input shaft, and control shaft requires external power (or braking power, if negative). Ratio of power sharing depends on gear ratio. If control shaft is locked ($n=0$), control power ($P_{control}$) is 0. Power sharing checked or not does not influence output power and torque in this case.



ZAR5: Wolf chart with torque, speed and power

Rotational speed and power at sun shaft (S), carrier (C) and hollow wheel (H) have been added to Wolf diagrams, and also planet gear transmission ratio $i0$ (zH/zS) and pitch power Pw .



Wolf chart for planet gear with connected input shaft and control shaft ($i=1$).

ZAR5 : Strength calculation for zero speed planet gear

If input shaft and control shaft are connected (i=1, n control = n input). Planet gear speed relative to carrier is 0 (npc=0). Fatigue strength of gear wheels could not be calculated in this case. Since release 10.0, ZAR5 calculates SH and SF as static safety coefficients from torque.

ZAR5: Screen graphic of gear pairs dimensions and strength calculation

ZAR5 - Planetary Gearing - ravign.z5

File Edit View CAD Database Document QLE Help

	1	2
z	16	47
d	48,000	141,000
db	45,105	132,497
da th	57,171	147,000
dNa	57,088	146,848
dNf	48,123	137,828
x	0,5284	0,0000
x mn	1,585	0,000
b	10,00	10,00
b eff	10,00	10,00
b0eff.	10,00	
kmm	0,000	0,000
en	3,558	4,712
et	3,558	4,712
zn	10,000	47,000
Asntol	e 25	e 25

	1 nom	1 min	1 max	2 nom	2 min	2 max
Asm	0,000	-0,060	-0,030	0,000	-0,108	-0,056
an	5,866	5,806	5,836	4,712	4,606	4,856
at	5,866	5,806	5,836	4,712	4,606	4,856
aan	1,206	1,134	1,170	2,388	2,278	2,328
aat	1,206	1,134	1,170	2,388	2,278	2,328
ave	0,52842	0,50095	0,51489	0,00000	-0,04854	-0,02564
q	0,000	0,000	0,000	0,000	0,000	0,000
qve	0,52842	0,50095	0,51489	0,00000	-0,04854	-0,02564
dew	48,762	48,753	48,771	143,238	143,212	143,264
df	43,671	43,606	43,668	133,500	133,209	133,348
dFf	45,592	45,524	45,557	135,872	135,492	135,676
da	57,088	57,006	57,068	146,848	146,709	146,848
dFa	57,088	57,006	57,068	146,848	146,709	146,848
dNa	57,088	57,006	57,068	146,848	146,709	146,848
c	0,783	0,765	0,810	0,783	0,765	0,810
h	6,750	6,709	6,701	6,750	6,681	6,619
jt	0°10'20"		0°25'12"	0°3'31"		0°9'36"
zeta a	0,831	0,831	0,832	0,553	0,533	0,556
zeta f	-1,237	-1,252	-1,139	-1,708	-1,715	-1,709

	nom	min	max
a	96,000	95,982	96,017
Aa	js 7	-0,018	0,018
Tsn		0,030	0,050
jt		0,073	0,179
alfa wt	22°19'49"	22°18'17"	22°21'20"
g alfa	12,678	12,405	12,725
g alfa A	4,445	4,251	4,479
g alfa E	8,234	8,155	8,245
eps alfa	1,432	1,401	1,437
eps gamma	1,432	1,401	1,437

	1	2
HP 0mm	1,000	1,000
HP 0ha	mm	3,000
HP 0mm	mm	1,250
HP 0hf	mm	3,750
raP 0mm	mm	0,250
raP 0hf	mm	0,750
rP 0mm	mm	0,000
rP 0ra	mm	0,000

	1	2
FpT	0,025	0,030
ftT	0,008	0,009
FalphaT	0,012	0,012
FbetaT	0,010	0,010
FalphaT	0,008	0,008
FbetaT	0,011	0,012
FbetaT	0,009	0,009
FbetaT	0,008	0,008
Fist	0,033	0,038
fsT	0,008	0,008
ftT	0,012	0,013
FrT	0,023	0,027

	nom	min	max
DM	3,400	3,400	3,400
MK nom	140,9905	140,9905	140,9905
MK max	140,795	140,795	140,795
MK min	140,617	140,617	140,617
k	3	3	3
VV nom	23,8976	23,8976	23,8976
VV max	23,869	23,869	23,869
VV min	23,841	23,841	23,841

	1	2
DM	4,100	4,100
MK nom	54,0475	54,0475
MK max	53,982	53,982
MK min	53,915	53,915
k	3	3
VV nom	23,8976	23,8976
VV max	23,869	23,869
VV min	23,841	23,841

error messages
Warning: SH<1 (1) (0,79)!

Same as in ZAR1+, you can now get screen with nom/min/max dimensions and strength calculation for gear pairs sun-planet and planet-ring gear.

ZAR5 - Planetary Gearing - ravign.z5

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CALCULATION METHOD: ISO 6336

	1	2	
Sigma-FG = SigmaFE * YNT * YdrelT * YRrelT * YX	MPa	532	847
Sigma-F0 = Ft / (b*mn) * YF * YS(g) * YB * YB * YDT	MPa	86	76
Sigma-F = Sigma-F0 * KA * Kv * KFB * KFAlfa	MPa	114	100
SF = Sigma-FG / Sigma-F	SF	4,668	8,484

	1	2	
Sigma-H0 = ZH * ZE * Zeps * ZB * sqrt(Ft / (d1*bt)*(u+1)u)	MPa	508	
Sigma-HG = SigmaHlim * ZNT * ZL * Zv * ZR * ZV * ZX	MPa	1441	1441
Sigma-HC = Sigma-H0 * sqrt(KA * Kv * KHb * KHAlfa)	MPa	616	
Sigma-H1,2 = (ZB_ZD) * Sigma-H0 * sqrt(KA * Kv * KHb * KHAlfa)	MPa	985	616
SH1,2 = Sigma-HG1,2 / Sigma-H1,2	SH	1,462	2,338

	1	2	
b eff	mm	10,00	10,00
mn	mm	3,000	
YF		1,225	1,293
sFn	mm	6,500	7,883
rhoF	mm	0,975	1,502
rHe	mm	2,983	4,270
alFen	°	26°54'9"	21°4'9"
xeF		0,52842	-0,52842
YS		2,523	2,091
qs		3,332	2,557
YB		1,000	
YDT		1,000	1,000
YdrelT		1,000	1,000
YRrelT		1,059	1,059
YX		1,000	1,000
Np		1	0
e		2	1
YA		0,83	1,00
YNT		1,00	1,00

	1	2	
b eff	mm	10,00	
df	mm	48,00	
Z		-5,000	
u		1,00	
ZNT		1,00	1,00
Zx		1,00	1,00

	1	2
KA H	1,00	
KA F	1,00	
Kv	1,00	
KH-beta	1,39	
KF-beta	1,26	
KH-alpha	1,06	
KF-alpha	1,06	

	1	2
ZH	2,49	
ZB	1,60	
ZE	190	
Z eps.	0,91	
Z beta	1,00	
ZL	1,00	
Zv	1,00	
ZR	0,96	
ZV	1,00	

	1	2
Ft	N	833
Ftw	N	833
Fxw	N	0
Frw	N	303
Fnw	N	887

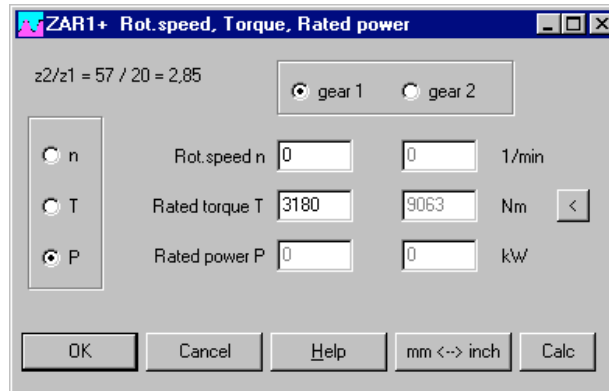
	1	2
K		
crowning	-	-
tapping-in/breaking-in	-	-
end relief	-	-
double helical gearing	-	-
supporting effect	-	-
tooth trace angle correction	-	-

	1	2	
RzZ	um	5,0	5,0
RzY	um	5,0	5,0
nue50	mm^2/a	100	
c gamma	N/mm	18,394	

	1	2
alpha t	20,00	
1	1,000	1,000
2	1,000	1,000

error messages
gear ratio!
Warning: Ft/b*KA < 100!

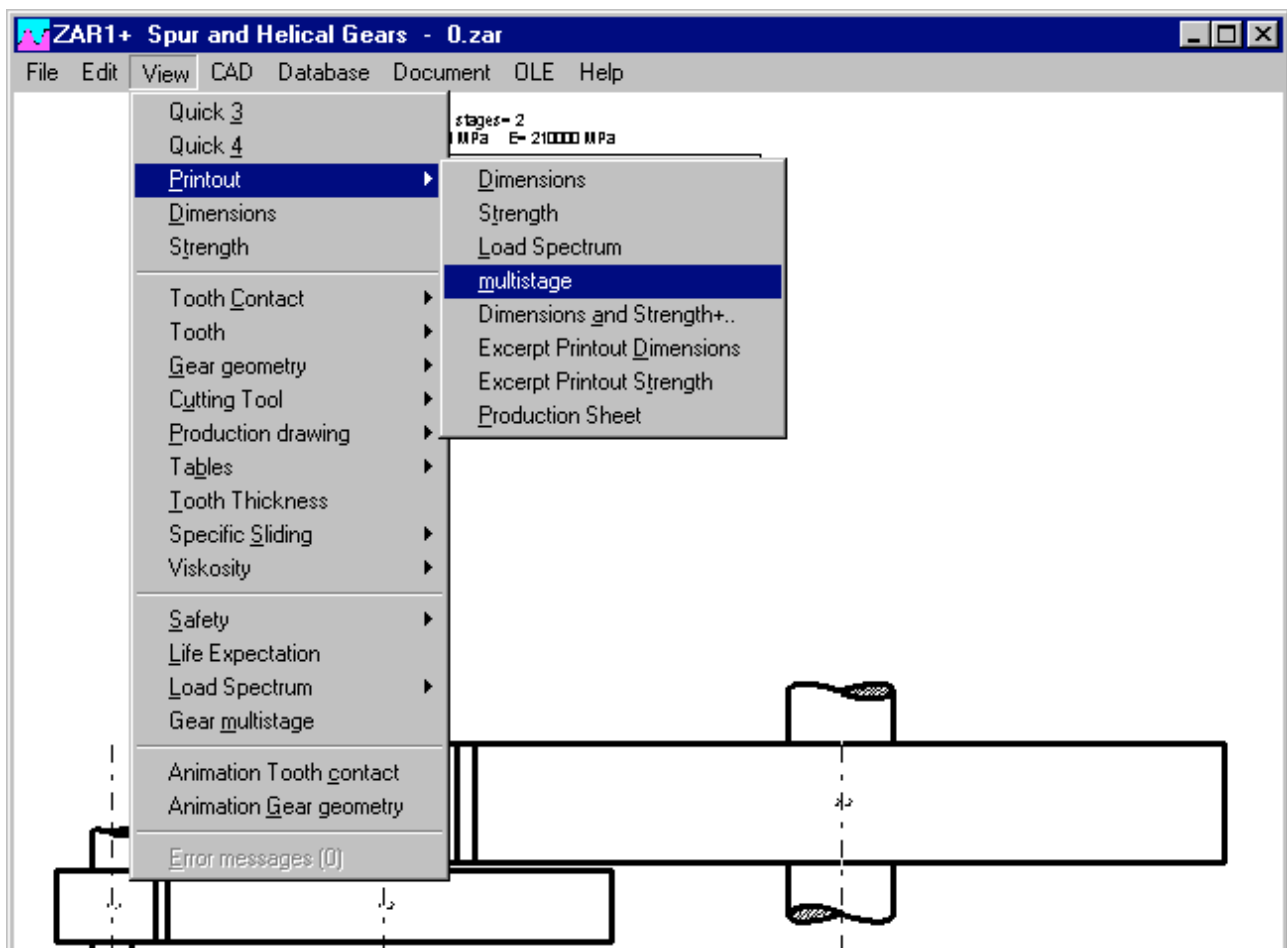
ZAR1+: Strength calculation for zero speed gear



In earlier versions, ZAR1+ calculated fatigue strength only if speed > 0 and power > 0 . Since release 25.0, ZAR1+ calculates static safety SH and SF for the given torque even if speed $n=0$.

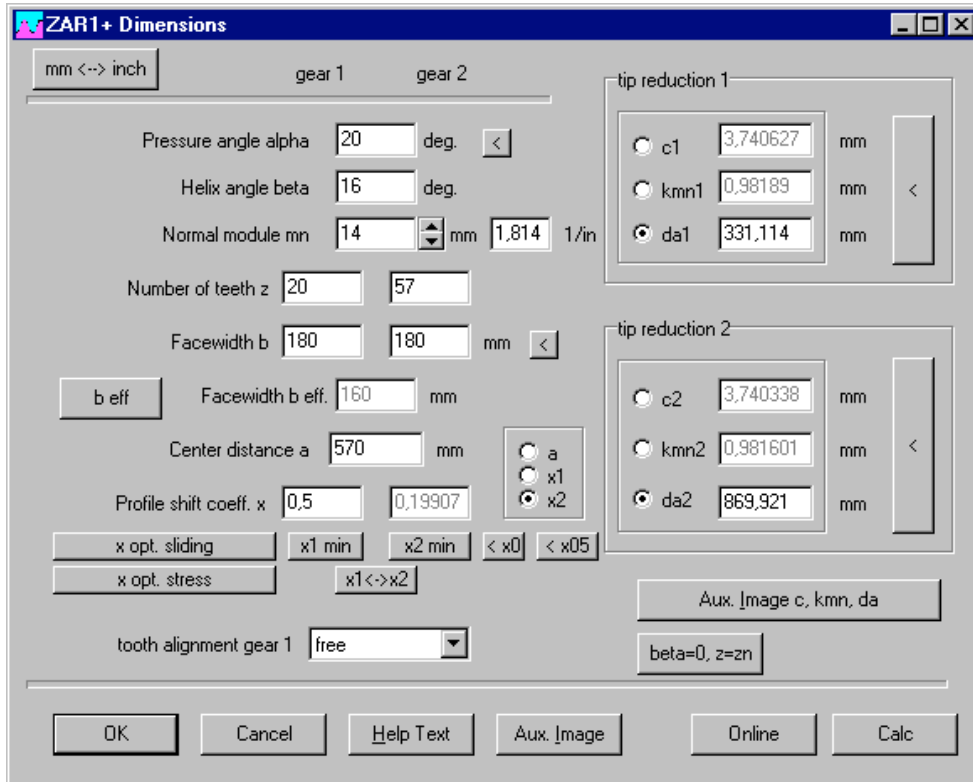
ZAR1+: Printout with load spectrum and multistage gear

Results of load spectrum calculation and multistage gear calculation can be printed separate now at "View->Printout"



ZAR1+, ZAR5: Edit Dimensions

Buttons x1min and x2min or xSmin and xPmin set minimum profile shift coefficient only if larger than 0. Else, x will be set 0.

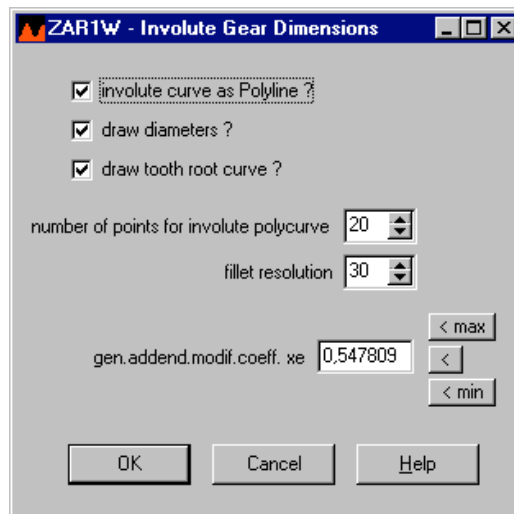


ZAR1+: Input profile shift and center distance

At input of gear pair dimensions you can select which one of the three values center distance, profile shift coefficient x1 or x2 should be calculated. Input has been optimized, selected value is calculated and shown now immediately after input of a, x1 or x2.

ZAR1W: CAD Tooth profile input window

As known from the involute spline programs, before generating the gear profile at "CAD->Tooth Profile Gear" you now get an input window with settings for profile shift coefficient or flank clearance, resolution of involute and tooth root curve, and drawing parameters.



FED1+,2+,3+,4, WN1, ZAR3+: Online Input with green and yellow fields

„Online Input“ is used for input windows with recalculated and updated results after each input step. Input fields are marked yellow now, if this field is a calculated value and input changes other input fields. So you are warned that input in a yellow field may change previous input data.

Input	Output
F2 60 N	R 2,265 N/mm
s2 22,15 mm	L0 40 mm
De 9,949 mm	Ln 75,02 mm
d 1,3 mm	Lk 26 mm
n(f) 19	tau k1 119,3 MPa
F0 9,829 N	tau k2 728,5 MPa
LH1 7 mm	tau kh 609,1 MPa
LH2 7 mm	tau perm 893,8 MPa
L2 62,15 mm	tau 0 99,12 MPa
	s1 0 mm
	s2 22,15 mm

A green input field means that the entered value is only approximate, it may be rounded or changed. This is the case for extension springs and torsion springs, where calculated number of coils must be rounded to loop position or leg angle, and the rest must be compensated by modified coil diameter.

Input	Output
ISO-A H 7	pu 56,84 MPa
ISO-I u 6	po 138,3 MPa
AαA 25 μm	SPI 3,089
AuA 0 μm	SPA 1,158
Aαl 76 μm	Uu 0,035 mm
Aul 60 μm	Uo 0,076 mm
Uu 0,035 mm	Tzul 755,0 Nm
Uo 0,076 mm	pnu 42,91 MPa
Rz-A 4 μm	Tu 1000 Nm
Rz-l 4 μm	SR 1,073
pmin 40 MPa	SPAx 2,14

Recalculation of cylindrical press fits with WN1 has many yellow fields: Input of ISO tolerances calculates tolerances A and then interference U of shaft and hub fit. Modification of tolerances A clears ISO tolerance. And modification of interference U clears all, tolerances A and ISO tolerances.

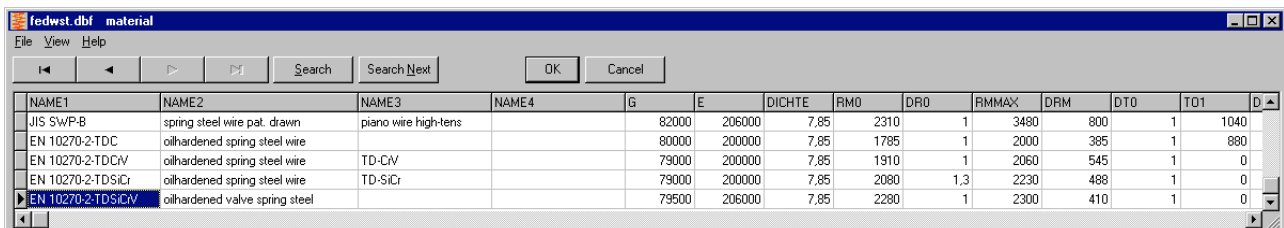
Spring material FD, TD, VD according to EN 10270-2

Old DIN 17223 defined material types FD for static and VD for dynamic load.

New EN standard defines FD for static load, TD for mean fatigue strength and VD for "difficult dynamic load". TD material types were not included in the fedwst material database as separate material until now. If your spring material database includes "TD" as second name in "Name3" or "Name4" of "VD" material, please clear "TD" at "Database->fedwst.dbf". Tensile strength and permissible shear stress of TD and VD is equal, but fatigue strength of TD is lower than VD.

EN 13906-1:2013 includes Goodman diagrams for TD (= FD) and VD. If these should be applied for FDC, TDC and VDC only, or also for FDCrV, FDSiCr, FDSiCrV, TDCrV, TDSiCr, TDSiCrV and VDCrV, VDSiCr and VDSiCrV, is not articulated. Fatigue strength data of VDSiCr and VDCrV used in fedwst.dbf is substantially higher than for VDC and originate from Bosch RDZ charts.

TDC, TDCrV, TDSiCr and TDSiCrV have been added in FEDWST.DBF now as separate materials. TDC with fatigue strength values of FDC and tensile strength parameters of VDC. No Goodman diagram is available for TDCrV, TDSiCr and TDSiCrV, but tensile strength is equal with VDCrV, VDSiCr and VDSiCrV.



NAME1	NAME2	NAME3	NAME4	G	E	DICHTE	RM0	DR0	RMMAX	DRM	DT0	TD1	D
JIS SWP-B	spring steel wire pat. drawn	piano wire high-tens		82000	206000	7,85	2310	1	3480	800	1	1040	
EN 10270-2-TDC	oilhardened spring steel wire			80000	200000	7,85	1785	1	2000	385	1	880	
EN 10270-2-TDCrV	oilhardened spring steel wire	TD-CrV		79000	200000	7,85	1910	1	2060	545	1	0	
EN 10270-2-TDSiCr	oilhardened spring steel wire	TD-SiCr		79000	200000	7,85	2080	1,3	2230	488	1	0	
EN 10270-2-TDSiCrV	oilhardened valve spring steel			79500	206000	7,85	2280	1	2300	410	1	0	

FED1+, 2+, 3+,5,6,7, 8: Temperature-dependant E modulus and G modulus

According to latest EN 13906-1 of 2013, spring wire to EN 10270-3 and to EN 12166 (bronze, copper alloy) are calculated with another temperature coefficient. New formula is used in our spring calculation software now.

$G = G20 * (1 - r * (t - 20))$ with $t =$ temperature in °C

$r = 0,25e-3$ for spring steel wire to EN 10270-1, EN 10270-2 and EN 10089

$r = 0,40e-3$ for spring steel wire to EN 10270-3

$r = 0,40e-3$ for spring wire to EN 12166

In earlier releases of EN 13906, a diagram instead of a formula was used to get temperature dependency. Converted into coefficient r , diagram values correspond to $r = 1/3600 = 0,28 e-3$.

Because formula was modified in the programs, you will get now slightly differing results when you load earlier calculations with operating temperature other than 20°C. If you open files in FED1+, number of coils is modified, spring loads remain unchanged. In FED2+, coil diameter may be modified, in FED3+ number of coils and delta0, in FED5, FED6 and FED7 the spring loads.

FED1+, 5, 6, 7: Reduced spring mass by grinding of spring ends

Grinded material of the end coils had not been considered in spring mass calculation, this was improved now.

FED5, FED6, FED7: Pitch height considered for calculation of wire length

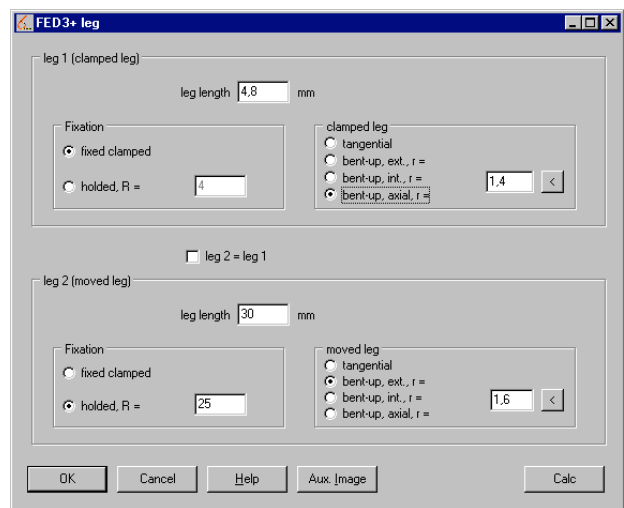
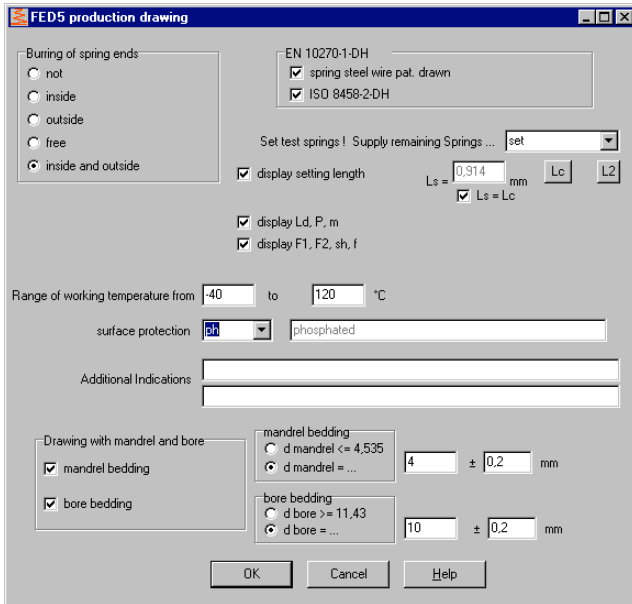
Same as already in FED1+, also FED5, FED6 and FED7 calculate wire length with consideration of spring height. In earlier versions, wire length was calculated simply as $\pi * D * nt$.

FED1+: Pitch m and swelling of the outside diameter deltaDe under load

In EN 13906-1:2013, calculation of pitch "m" for calculation of deltaDe was corrected (19). In FED1+ and FED6, coil pitch „m“ („P0“ in FED1+) since years is calculated to the new formula: $m = (L0-Lc)/n+d$ (see info 121). This is equal with the new formula in EN: $m = (sc + n*d)/n$. More simply it should be: $m = sc/n + d$. However, this formula is valid also for compression springs with raw spring ends. The other formula " $m=(sc+(n+1.5)*d)/n$ " in EN 13906 is superfluous and wrong, cause difference for raw end coils is already included in block deflection sc.

FED1+, FED5, FED6: Dimensions of mandrel and bore separate

Fields for mandrel and bore have been separated in the production drawing input window to avoid overlap when define spring led by both, mandrel and bore.

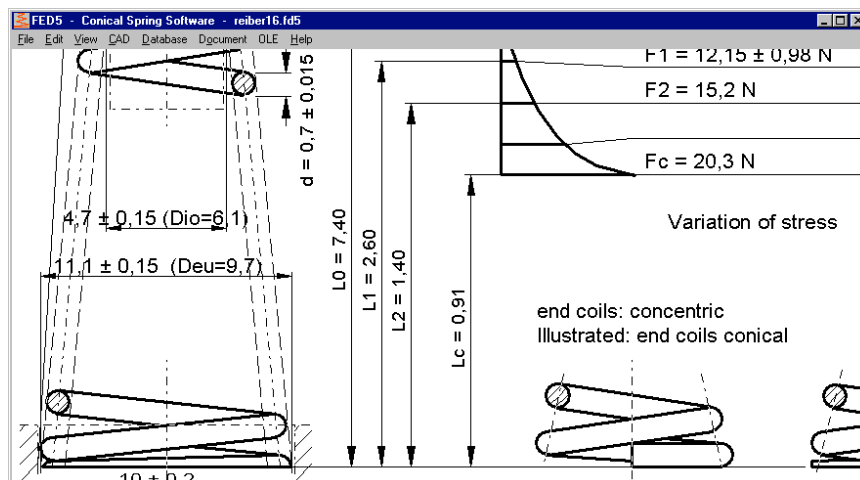


FED3+ Legs bent-up, axial

Legs can be tangential or bent-up external, internal, or axial (new).

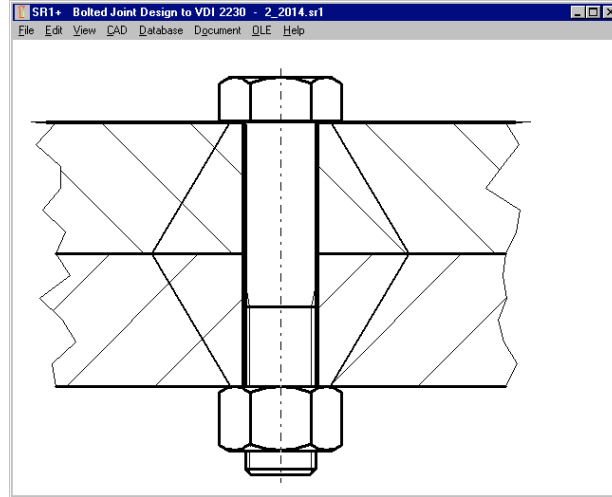
FED5: Concentric end coils

If concentric end coils defined, FED5 production drawing includes dimensions of minimum inside diameter and maximum outside diameter of the end coils instead of coil diameters (coil diameters Dio and Deu in brackets). Production drawing always illustrates conical end coils.



SR1+: Calculate deformation cone of TTJ with TBJ calculation method

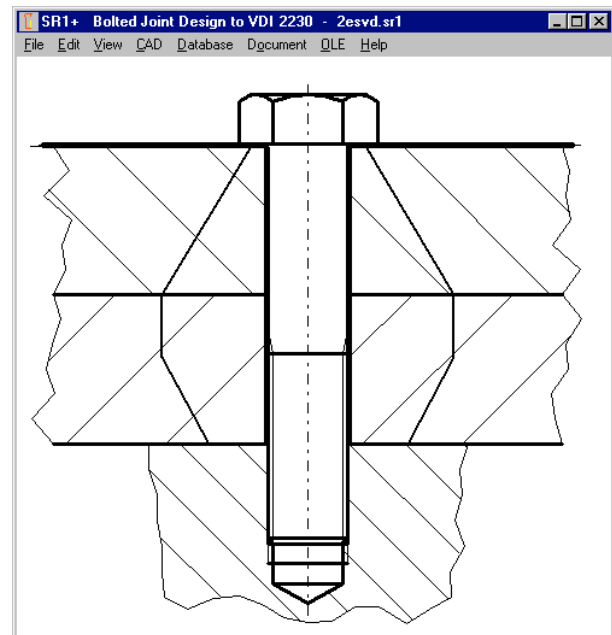
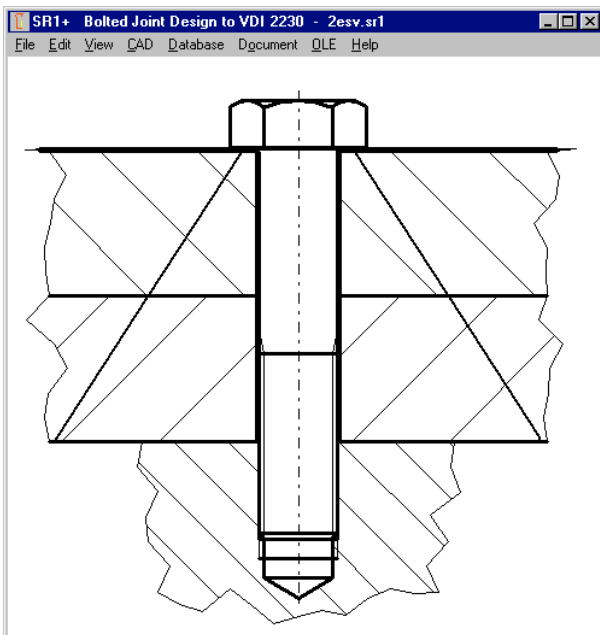
VDI 2230 differs calculation of deformation cone between TTJ and TBJ. In figure 9, deformation cones are illustrated (a), but VDI 2230 uses one deformation cone followed by a sleeve "to simplify the calculation". This calculation method is not applicable for a bolted joint of several clamping plates with more than one deformation cone. But even for simple calculations, this simplified calculation method seems to be incorrect. Example: B2 of VDI 2230



Supposed a tapped thread joint (TTJ) instead of through-bolt joint (TBJ). Then calculate cone angle $\tan(\phi_E) = 0.348 + 0.013 \cdot \ln(BL) + 0.193 \cdot \ln(y) = 0.647$ ($\phi = 32.8^\circ$, larger than ϕ_D of TBJ!)

$DA, Gr = dw + 2 \cdot k \cdot \tan(\phi) = 100 \text{ mm}$ (larger than TBJ!)

Comparing the deformation bodies of TTJ joint and equivalent TBJ joint shows that there must be something wrong: The TTJ deformation body is only one huge cone, because "DA,Gr" nor "de" will be reached.

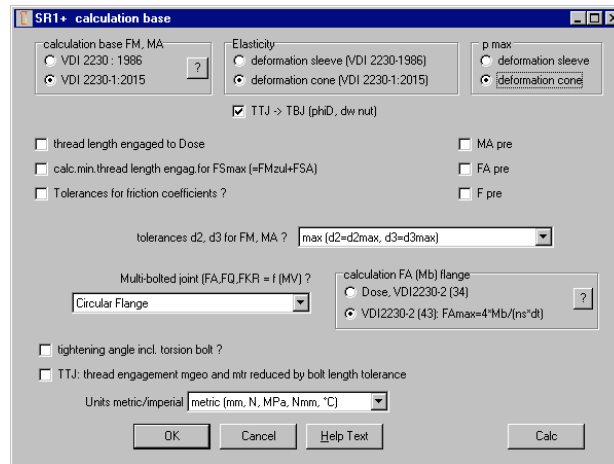


In SR1+ you can now set the option „TTJ -> TBJ (ϕ_D , dw_{Nut})“ to calculate the deformation body of the TTJ in the same way as for TBJ. SR1+ calculates bearing diameter of the female thread according to figure 9 of VDI 2230-1:2015 ($dw = d + 2 \cdot \tan(\phi_D) \cdot m_{geo}$ with m_{geo} = screw-in depth of bolt in female thread, possibly less one thread pitch).

Because cone angle ϕ depends on bearing diameter dw and vice versa, dw and ϕ_D are calculated iterative.

SR1+: Calculate pressure from deformation cone cross-section

In earlier versions of SR1, pressure F/A between clamping plates was calculated with virtual external diameters according to VDI 2230:1986. At „pmax“ you now can calculate pressure from section area of the deformation cones. If TTJ, better set „TTJ -> TBJ (phiD, dwnut)“, else you may get too large cross-section area resulting in too low pressure. In most cases, flank pressure safety margin remains the same, because maximum value applies between bolt head or washer and first clamping plate, or between nut and last clamping plate.



SR1+: Non-standard sizes added for hexagon head bolts

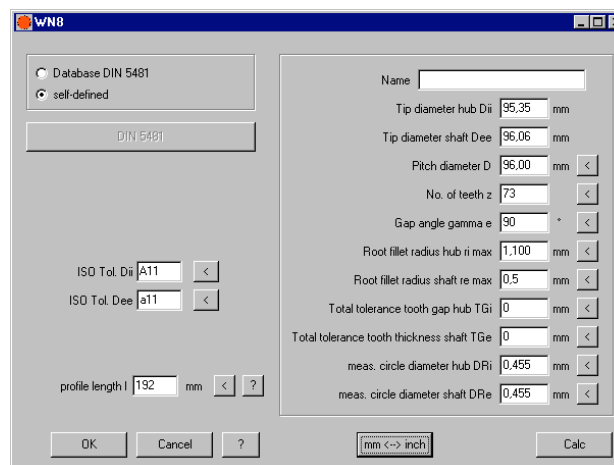
Sizes M45, M52, M60, M68 and M160 added in the database (according to DIN 931).

SR1+: Safety not shown if $S > 1000$

At Quick3 View, Quick4 View, and table drawing, safety margins are listed only if less than 1000.

WN8: ISO tolerance for self-defined splines

For self-defined splines you can now input ISO tolerance for tooth tip diameter of internal and external spline. If nothing entered, diameters are calculated without tolerance. If you select profile from DIN 5481 database, ISO tolerance A11 will be set for internal spline and a11 for external spline. In self-defined splines, root fillet radius can be set 0 now. In earlier versions, maximum fillet radius was calculated in this case.



Involute spline package

For calculation of involute splines to different standards DIN 5480, ANSI B92.1, ISO 4156, DIN 5482 and self-defined involute splined joints, we offer now a bundle with WN2+, WN4, WN5, WN10 and WNXE for a price of 1200 Euro.

PRICELIST 2016-03

PRODUCT	EUR
DI1 Version 1.2 O-Ring Seal Software	190,-
DXF-Manager Version 8.7	383,-
DXFPLOT V 3.2	123,-
FED1 V28.1 Helical Compression Springs	491,-
FED1+ V28.1 Helical Compression Springs incl. spring database, animation, relax., 3D,..	695,-
FED2 V19.6 Helical Extension Springs	501,-
FED2+ V19.6 Helical Extension Springs incl. spring database, animation, relaxation, ...	675,-
FED3+ V18.2 Helical Torsion Springs incl. prod.drawing, animation, 3D, rectang.wire, ...	480,-
FED4 Version 7.2 Disk Springs	430,-
FED5 Version 15.0 Conical Compression Springs	741,-
FED6 Version 15.5 Nonlinear Cylindrical Compression Springs	634,-
FED7 Version 12.4 Nonlinear Compression Springs	660,-
FED8 Version 6.7 Torsion Bar	317,-
FED9 Version 5.8 Spiral Spring	394,-
FED10 Version 3.3 Leaf Spring (complex)	500,-
FED11 Version 3.3 Spring Lock and Bushing	210,-
FED12 Version 2.4 Elastomere Compression Spring	220,-
FED13 Version 3.9 Wave Spring Washers	185,-
FED14 Version 1.4 Helical Wave Spring	395,-
FED15 Version 1.3 Leaf Spring (simple)	180,-
GEO1+ V5.7 Cross Section Calculation incl. profile database	294,-
GEO2 V2.6 Rotation Bodies	194,-
GEO3 V3.3 Hertzian Pressure	205,-
GEO4 V3.9 Cam Software	265,-
HPGL-Manager Version 8.6	383,-
LG1 V6.4 Roll-Contact Bearings	296,-
LG2 V2.1 Hydrodynamic Plain Journal Bearings	460,-
SR1 V21.2 Bolted Joint Design	640,-
SR1+ V21.2 Bolted Joint Design incl. Flange calculation	750,-
TOL1 V11.8 Tolerance Analysis	506,-
TOL1CON V1.5 Conversion Program for TOL1	281,-
TOL2 Version 3.3 Tolerance Analysis	495,-
TOLPASS V4.1 Library for ISO tolerances	107,-
TR1 V3.8 Girder Calculation	757,-
WL1+ V19.8 Shaft Calculation incl. Roll-contact Bearings	945,-
WN1 Version 11.6 Cylindrical and Conical Press Fits	485,-
WN2 V 9.5 Involute Splines to DIN 5480	250,-
WN2+ V 9.5 Involute Splines to DIN 5480 and non-standard involute splines	380,-
WN3 V 5.3 Parallel Key Joints to DIN 6885, ANSI B17.1, DIN 6892	245,-
WN4 V 4.4 Involute Splines to ANSI B 92.1	276,-
WN5 V 4.4 Involute Splines to ISO 4156 and ANSI B 92.2 M	255,-
WN6 V 2.9 Polygon Profiles P3G to DIN 32711	180,-
WN7 V 2.2 Polygon Profiles P4C to DIN 32712	175,-
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WN10 V 3.7 Involute Splines to DIN 5482	260,-
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Updates:

Update prices	EUR
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Software Update (software 64-bit Win + pdf manual)	50,-

Update Mechanical Engineering Package: 800 EUR, Update Complete Package: 1000 EUR

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